ature, the complete system can be described up to the critical point.

Figure 1 illustrates the P-T relations for the system. The solid line for *n*-pentane was drawn by using literature data while the points on that line correspond to experimental check data on that component.

Figure 2 illustrates the P-T projections of the bubble points of the three mixtures calculated with the Peng-Robinson (2) equation and experimental measurements from this study. As can be seen, the Peng-Robinson equation is able to predict bubble points of this system satisfactorily. No binary interaction coefficients were used in this study.

Registry No. n-Pentane, 109-66-0; pent-1-ene, 109-67-1.

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Viscosities and Densities of Binary Mixtures of 1-Alkanois from 15 to 55 $^{\circ}$ C

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Viscosities of binary mixtures of 1-decanol, 1-nonanol, 1-octanol, and 1-heptanol with 1-butanol, 1-propanol, ethanol, and methanol were measured at 15, 25, 35, 45, and 55 °C. Viscosities η are presented as a polynomial in mole fraction X_1 of the low molecular weight component of binary mixture: $\eta = A + BX_1 + CX_1^2 + DX_1^3 + EX_1^4$. Molar volumes of binary mixtures are given by the sums of the products of molar volume and mole fraction of components involved. Viscous heats and preexponential factors are also reported. These data were also fitted to the empirical equation of McAllister, Herric, Auslander, and two additional polynomials.

Introduction

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The literature dealing with the viscosity of mixtures of 1-alkanols is rather limited. While a number of empirical relations (1-6) have been proposed to predict the viscosity of a mixture from that of pure components, we did not trust the extrapolation to higher alkanols. In the present work, we have measured the viscosity of 16 binary mixtures comprising 1-decanol, 1-nonanol, 1-octanol, 1-heptanol, 1-butanol, 1-propanol, ethanol, and methanol. These data were fitted to a five-parameter polynomial with a goodness of fit approximating experimental error. In addition, these binary data were fitted to the empirical relations of McAllister (1), Herric (2), and Auslander (3) and also to two additional polynomial equations using a multiparametric curve-fitting program. In order to obtain viscosity from kinematic viscosity, densities of all mixtures were also determined. The viscous heat and the preexponential factor of the mixtures were also calculated.

Models and Equations

Several equations have been put forward to calculate the viscosities of binary mixtures.

McAlitister's Formula (1). McAllister derived the following relation for a liquid mixture on the basis of the absolute reaction rate theory of Eyring:

$$\ln \eta = X_1^3 \ln \eta_1 + 3X_1^2 X_2 \ln \eta_{12} + 3X_1 X_2^2 \ln \eta_{21} + X_2^3 \ln \eta_2 + D'$$
(1)

 $D' = -\ln (X_1 + X_2M_2/M_1) + 3X_1^2X_2 \ln (\frac{2}{3} + M_2/3M_1) + 3X_1X_2^2 \ln (\frac{1}{3} + 2M_2/3M_1) + X_2^3 \ln (M_2/M_1)$

The equation contains two adjustable parameters, in $\eta_{\rm 12}$ and $\ln\,\eta_{\rm 21}.$

Herric's Formula (2). The following relation was proposed by Herric to correlate viscosities of binary mixture:

$$\ln \eta = X_1 \ln \eta_1 + X_2 \ln \eta_2 + X_1 \ln M_1 + X_2 \ln M_2 - \ln (X_1 M_1 + X_2 M_2) + \Delta 12 (2)$$

where $\Delta 12 = \alpha_{12} X_1 X_2$ is a function representing molecular interaction and $\alpha_{12} = \alpha_{21}$ is the interaction parameter. Herric expressed α_{12} or α_{21} as a linear function of composition

$$\alpha_{12} = \beta_{12} + \beta_{21}(X - X_2) \tag{3}$$

The coefficients β_{12} and β_{21} may be determined from a least-squares method.

Auslander's Formula (3). Auslander's equation has the following three-parameter form:

$$X_{1}(X_{1} + B_{12}X_{2})(\eta - \eta_{1}) + A_{21}X_{2}(B_{21}X_{1} + X_{2})(\eta - \eta_{2}) = 0$$
(4)

Here, A_{21} , B_{12} , and B_{21} are the parameters representing binary interactions.

Polynomial Functions. Viscosity data were fitted to three different polynomials of the following form, the first of which was chosen as the form of data presentation in this paper; note that polynomial I is the only equation which does not require fixed values of the viscosities of the pure components and allow them to share in the goodness of fit:

polynomial I

$$\eta = A + BX_1 + CX_1^2 + DX_1^3 + EX_1^4 \tag{5}$$

where A, B, C, D, and E are adjustable parameters. polynomial II

$$\eta = \eta_1 X_1 + \eta_2 X_2 + A X_1 + B X_2 + X_1 X_2 A + B(X_1 - X_2) + C(X_1 - X_2)^2$$
(6)

polynomial III

$$\eta = \eta_1 X_1 + \eta_2 X_2 + X_1 X_2 A + B(X_1 - X_2) + C(X_1 - X_2)^2$$
(7)

	15.0 °C		25.0 °C		35.0 °C		45.0 °C,	55.0 °C
	obsd	lit.	obsd	lit.	obsd	lit.	obsd	obsd
				0.7865 ^a				
C1	0.7959	0.7960 ^e	0.7861	0.7864 ^b	0.7755		0.7693	0.7586
•1				0.7866 ^c				
C.	0.7934	0.7933 ^e	0.7845	0.7850 ^c	0.7767	0.7764 ^e	0.7681	0.7599
C ₂ C ₃	0.8077	0.8075 ^e	0.7994	0.8023^{d}				
0,				0.7993 ^e	0.7920		0.7841	0.7758
C₄	0.8132	0.8133 ^e	0.8056	0.8085^{d}				
-4				0.8057 ^a	0.7981		0.7907	0.7829
C.	0.8257		0.8190		0.8112		0.8041	0.7871
Č.	0.8276	0.8320 ^e	0.8211		0.8142		0.8078	0.8010
Ċ.	0.8310		0.8244		0.8177		0.8111	0.8043
$\begin{array}{c} C_7 \\ C_8 \\ C_9 \\ C_{10} \end{array}$	0.8327		0.8254		0.8197		0.8127	0.8064

Table I. Densities (g/mL) of Different 1-Alkanols

^a Reference 8. ^b Reference 9. ^c Reference 10. ^d Reference 11. ^e Reference 12.

Table II. Viscosities (cP) of 1-Alkanols

	15.0 °C		25.0 °C		35.0 °C		45.0 °C		55.0 °C,
	obsd	lit.	obsd	lit.	obsd	lit.	obsd	lit.	obsd
C ₁	0.6305		0.547	0.546 ^a 0.545 ^{b,c}	0.4745		0.4194		0.3722
C ₂	1.280		1.056	$1.078^d \\ 1.068^e$	0.8818	0.8683 ^e	0.7461	0.7292 ^e	0.6302
C,	2.3179	2.522^{d}	1.898	1.966^{f} 2.577^{h}	1.436		1.223		0.9908
C₄	3.159	3.379 ^e	2.524	2.564^{f} 2.463^{g}	1.969	2.00^{i}	1.558		1.246
с.	8.302		5.774		4.263		3.156		2.364
Ċ,	10.662	10.640 ^e	7.363	7.21^{d}	5.256		3.868		2.890
C ₇ C ₈ C ₉	13.146		9.101		6.522		4.677		3.476
C_{10}^{j}	16.465		10.974		7.509		5.358		3.957

^a Reference 13. ^b Reference 14. ^c Reference 15. ^d Reference 16. ^e Reference 12. ^f Reference 11. ^g Reference 17. ^h Reference 18. ⁱ Reference 19. ^j The interpolated values of viscosities at 11 and 32 °C from the present data are in good agreement with ref 20.

Table III. Averages of Rms for All Mixtures at All Temperatures of 1-Alkanol

					polynomial	
	McAllister ^a	Auslander	Herric ^a	I	II	III
C ₁₀ mixtures	0.0258	0.0410	0.0378	0.0417	0.2442	0.0576
C_7 mixtures	0.0200	0.0118	0.0138	0.0130	0.1161	0.0122

^a Rms in logarithm form.

Here again, A, B, and C are adjustable parameters and could be determined by a weighted least-squares method.

The viscous heat and the preexponential factor of the mixtures were also calculated from the equation

$$\eta = \eta_0 \exp(E_v/RT) \tag{8}$$

where η is viscosity, η_0 is the preexponential factor, E_v is viscous heat, R is the gas constant, and T is the absolute temperature.

Experimental Section

All 1-aikanols used in this work were of analytical grade (Fluka AG, Buchs SG) and had a purity of 99.9%. Mixtures of methanol, ethanol, 1-propanol, and 1-butanol with 1-heptanol, 1-octanol, 1-nonanol, and 1-decanol were prepared in all compositions used by weighing an appropriate volume of each solvent. Density and viscosity measurements were carried out at five different temperatures, i.e., 15.0–55.0 °C with a regular interval of 10 °C.

Density measurements were carried out by using a densitometer which was calibrated with mercury. The densitometer was a specific gravity bottle (~ 10 mL) which had a graduated capillary neck. Viscosities of mixtures were determined by KPG-Ubbelhode viscometers, Schott-Gerate Nos. 2450113, 2452610, and 2452613. Time of flow was noted by using the Model AVS viscosity measuring instrument of Schott-Gerate, which uses a modulated light transmitter/receiver. Efflux times are noted by a digital counter of 0.01-s resolution.

A temperature stability of ± 0.1 °C was recorded by using a platinum resistance thermometer. Computation of the kinematic viscosity is done by using the relation

 $\alpha = kt$

where α = kinematic viscosity of a sample in cSt, k = capillary constant of the viscometer in cSt/s, and, t = time of flow in seconds.

The viscometer was calibrated with water at all working temperatures and the mean value of k was used in calculations.

The kinematic viscosities were adjusted for kinetic energy by using the Hagenbach correction (7). Absolute viscosity values were then determined by using the relation

$$\eta = \alpha \rho$$

where η = absolute viscosity of a sample in cP and ρ = density of a sample in g/mL.

Results and Discussion

Densities were determined for pure 1-alkanois C_1 , C_2 , C_3 , C_4 , C_7 , C_8 , C_9 , and C_{10} at 15, 25, 35, 45, and 55 °C. The values are listed in Table I along with literature values and there is

Table IV. Values of Various Parameters for the Equation $\eta = A + BX_1 + CX_1^2 + DX_1^3 + EX_1^4$

emp, °C	A	В	<u> </u>	D	<i>E</i>	rms error
			Methanol-De			
15.0	16.487	-19.236	-16.217	32.563	-12.990	0.09841
25.0	10.980	-11.592	-8.454	14.123	-4.5066	0.04011
35.0	7.5093	-7.2678	-3.6477	4.3907	-0.5008	$0.037\ 20$
45.0	5.358 6	-4.3030	-3.2140	2.4981	0.086 15	0.03035
55.0	3.9729	2.7724	-28.990	41.400	-19.002	0.09052
			Ethanol-Dec	canol		
15.0	16.4660	-18.3378	-9.4225	19.874 1	-7.3129	0.0225711
25.0	10.9748	-10.8795	-5.45122	8.967 3	-2.55745	0.010 266 9
35.0	7.51260	-3.2719	-21.2750	31.9170	-14.0239	0.058139
45.0	5.356 76	-11.2944	23.6193	-29.0041	12.1350	0.052669
55.0	3.95976	-3.156 47	-3.34779	6.794 59	-3.621 97	0.040676
			Propanol-De	canol		
15.0	16.4666	-13.7138	-12.5778	19.426 3	-7.269 92	0.02220
25.0	10.9753	-8.85244	-4.57148	5.456 26	-1.11185	0.008225
35.0	7.51060	-6.24876	3.24705	-4.249 88	2.165 10	0.05286
45.0	5.35582	-4.32280	0.206155	0.905 682	0.910139	0.02829
55.0	3.954 61	-2.88533	-0.42544	0.087 336	0.276 58	0.02385
			Butanol-Dec	canol		
15.0	16.4651	-13.5719	-11.0718	19.1023	-7.7476	0.022732
25.0	10.9744	-6.269 33	$-17.152\ 2$	26.2697	-11.336 5	0.076374
35.0	7.51470	-7.72269	6.320 51	-8.30482	4.16757	0,79977
45.0	5.360 10	-4.49591	1.42237	-2.39371	1.650 94	0.024 030
55.0	3.958 59	-3.218 39	1.15352	-1.857 40	1.193 89	0.017 058
			Methanol-No	nanol		
15.0	13.1583	-16.6891	-6.424 56	17.718 2	-7.14416	0.027524
25.0	9.108 03	-11.9411	1.387 29	2.333 26	-0.34657	0.027 829
35.0	6.526 32	-7.61165	-0.185159	2.139 81	-0.405364	0.022 096 8
45.0	4.679 21	-4.75938	-0.415014	0.649 477	0.260 209	0.007 096 6
55.0	3.468 63	-2.37448	-3.27572	3.54674	-0.999 072	0.028679
			Ethanol-Noi	anol		
15.0	13.1439	-13.1526	-4.82837	8,450 35	-2.30347	0.379 53
25.0	9.098 84	-9.34524	0.342 402	0.307 139	0.678 855	0.351 205
35.0	6.521 40	-6.667 31	1.976 85	-2.47360	1,54313	0.023070
45.0	4.676 38	-4.08619	0.643 39	-1.53851	1.060 3	0.014 490 5
55.0	3.475 87	-2.8555	0.50370	-1.12162	0.633 199	0.007 500 2
			Propanol-No	nanol		
15.0	13.1489	-10.404 7	-9.725 2	15.4717	-6.157 07	0.029 722
25.0	9.102 25	-8.395 02	-0.17242	2.081 26	-0.780 816	0.024 729
35.0	6.522 03	-6.20787	2.048 91	-1.601 89	0.696 724	0.018 149 8
45.0	4.67849	-4.004 09	1.806 39	-2.88277	1.621 30	0.007 182 6
55.0	3.47672	-2.762 31	1.18416	-2.01291	1.102 64	0.004 329 0
			Butanol-Noi	nanol		
15.0	13.1356	-11.9528	0.576 935	1.719 58	-0.277 45	0.045578
25.0	9.095 89	-9.341 59	6.364 09	-7.03012	3.443 02	0.020 389
35.0	6.515 51	-6.991 90	7.03372	-8.556 63	3.977 49	0.027 730
45.0	4.669 03	-3.67017	-0.048921	1.101 71	-0.49312	0.056 225
55.0	3.47377	-3.0830	2.94513	-3.97466	1.887 66	0.008 629
			Methanol-Oc	tanol		
15.0	10.663 0	-17.009 2	7.911 30	-1.5734	0.627 403	0.014548
25.0	7.363 81	-10.3300	3.65887	-0.644 49	0.493 51	0.008 161 5
35.0	5.256 29	-6.360 68	1.267 23	-0.040 657	0.349 462	0.006 075
45.0	3.868 80	-4.10405	0.48482	-0.337 46	0.505 059	0.004 896 8
55.0	2.890 99	-2.63268	-0.010 37	-0.332 29	0.453 40	0.003 431 1
			Ethanol-Oc	tanol		
15.0	10.6623	-14.1801	3.340 31	3.3220	-1.856 42	0.010 532
25.0	7.36145	-9.256 48	4.07724	-2.095 89	0.987 38	0.018673
35.0	5.25600	-5.21716	-0.686 48	2.57646	-1.04193	0.004 136 8
45.0	3.868 60	-3.590 05	-0.05427	0.749961	-0.225139	0.0024367
55.0	2.890 76	-2.369 19	-0.25364	0.459 664	-0.096 460	0.001 383 0
			Propanol-Oc	tanol		
15.0	10.6650	-10.461 7	-0.532 237	5.438 25	-2.78278	0.049887
25.0	7.361 28	-6.79471	1.17285	0.443472	-0.343 69	0.022588
35.0	5.252 59	-7.22041	12.0822	-14.8039	6.14786	0.029 603
45.0	3.871 93	-3.309 94	1.56908	-1.63167	0.717 563	0.033235
55.0	2.89264	-3.393 71	5.90674	-7.86073	3.446 90	$0.027\ 647$
			Butanol-Oct	anol		
	10 000 4	-9.851 35	2.01369	1.401 64	-1.03886	0.028 599
15.0	10.6604			1.101 01	1.000.00	0.020000
15.0 25.0 35.0	7.363 70	-6.14710 -3.98103	1.60414 0.862344	-0.805 49	0.505 984	0.003 685

temp, °C	A	В	С	D	${oldsymbol E}$	rms error
45.0	3.868 97	-2.733 36	0.689 260	-0.629 644	0.359 875	0.005 133 5
55.0	2.892 96	-1.71408	-0.213536	0.338 578	-0.062 032	0.009 402 6
			Methanol-Hep	otanol		
15.0	8.302 12	-14.1532	9.853 54	- 5.098 60	1.71948	0.007265
25.0	5.77425	-8.080 30	3.31836	-0.941 969	0.47238	0.005676
35.0	4.263 39	-5.45785	1.966 28	-0.64972	0.349 635	0.002859
45.0	3.145~70	-3.45383	0.97397	-0.87164	0.623 356	0.006 198 7
55.0	2.36467	-2.06066	-0.268275	0.202 856	0.130 148	0.003283
			Ethanol-Hep	tanol		
15.0	8.299 35	-11.3512	5.343 21	-0.50866	-0.477 709	0.023642
25.0	5.77304	-6.373 35	0.598 299	2.40672	-1.331 62	0.013434
35.0	4.26234	-4.52716	0.949 560	$0.710\ 248$	-0.498834	0.0121202
45.0	3.153 95	-2.47982	-2.02238	4.22071	-2.105 31	0.046015
55.0	2.36465	-1.66282	-0.871664	1.366 76	-0.561 34	0.006 303 3
			Propanol-Hep	otanol		
15.0	8.299 93	-8.38526	3.450 22	-0.714618	-0.30720	$0.027\ 027$
25.0	5.773 56	-4.31971	-1.10253	3.084 36	-1.60427	0.016 135 3
35.0	4.261 94	-3.50908	1.27557	-0.549 53	-0.026 697	0.016 629 7
45.0	3.157 26	-2.31546	1.10516	-1.507 96	$0.782\ 215$	0.004 578 7
55.0	2.36687	-1.16939	-0.87457	1.000 99	$-0.339\ 387$	0.0094348
			Butanol-Hep	tanol		
15.0	8.295 47	-7.04588	2.743 06	-0.32491	-0.501 93	0.02343
25.0	5,775 01	-3.781 99	0.058 004	0.762 847	-0.290 86	0.0031523
35.0	4.264 05	-3.198 57	2.344 56	-2.51275	1.072 89	0.012 013 6
45.0	3.157 40	-1.93782	0.866140	-0.962614	0.434 913	0.0120628
55.0	2.36647	-1.16918	0.074282	-0.129 261	0.100 427	0.0091420

agreement to three significant figures. The estimated error in densities was $\pm 2 \times 10^{-5}$ g/mL. The good agreement of the experimental values of density with literature values allows the report of absolute viscosities instead of kinematic viscosities. The experimental values of absolute viscosities for the pure alkanols are reported at five temperatures in Table II, along with literature values for comparison. Observed viscosity values fall within the ranges of those reported in the literature. Literature values of C₇, C₉, and C₁₀ were not available for these temperatures; however, interpolated data were in good agreement with the values reported in the literature (see footnotes to Table II). The estimated error of measurement in viscosities was 1 \times 10⁻⁴ cP.

Viscosities of binary mixtures of 1-alkanols were fitted to McAllister, Auslander, and Herric's equations and also to three polynomials. The average values for the root mean square (rms) for all mixtures of C_{10} and C_7 investigated are given in Table III. The rms values of McAllister and Herric equations are for the natural logarithm of the rms, whereas that of Auslander's is in terms of viscosities and thus cannot be compared directly. A reasonable fit was found for all equations. A detailed table of rms values is available as supplementary material (see paragraph at end of text regarding supplementary material). It should be noted that all equations tested except polynomial I included fixed end values such that the experimental values of the pure components do not participate in the error determination.

The viscosities of binary mixtures at each temperature are reported in terms of the parameters of polynomial I in Table IV. It should be noted that parameter A is the best fit absolute viscosity for the high molecular weight component of the binary mixture whereas the sum of the other four parameters is the best fit value of the absolute viscosity of the low molecular weight component. This polynomial allows the calculation of viscosities of any mole fraction of the mixture within the rms error reported.

The ideal behavior of the molar volumes of the binary mixture of 1-alkanols as reported by $\bar{V} = X_1 \bar{V}_1 + X_2 \bar{V}_2$ is illustrated for two binary mixtures in Figure 1, where the molar volume is plotted vs. mole fraction. Viscous heats and preexponential factors as derived from the viscosities given by eq 8 are

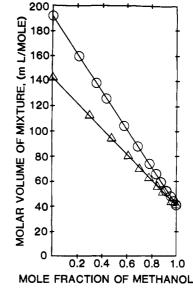


Figure 1. Molar volume of mixture vs. mole fraction of C_1 in binary mixtures of 1-alkanols: (O) C_1 - C_{10} ; (Δ) C_1 - C_7 .

Table V. Viscous Heats (E_v) and Preexponential Factors (η_0) of Various 1-Alkanols

	$E_{\rm v}$, kc	al/mol	$10^{3}\eta_{0}, cP$		
	obsd	lit. ^a	obsd	lit.ª	
$\overline{C_1}$	2.50 ± 0.01	2.46 ± 0.04	8.2 ± 0.3	8.65	
C_2	3.29 ± 0.01	3.22 ± 0.13	4.2 ± 0.4	4.65	
C ₃	3.91 ± 0.08	4.27 ± 0.28	2.56 ± 0.25	1.46	
C₄	4.37 ± 0.05		1.64 ± 0.23		
C,	5.85 ± 0.03		0.38 ± 0.08		
C _s	6.04 ± 0.02		0.276 ± 0.044		
$ \begin{array}{c} C_1 \\ C_2 \\ C_3 \\ C_4 \\ C_7 \\ C_8 \\ C_9 \end{array} $	6.17 ± 0.02		0.273 ± 0.025		
C10	6.67 ± 0.04		0.153 ± 0.017		

^a Reference 21.

presented in Table V. Viscous heats (SD = ± 0.03 kcal/mol) and preexponential factors (SD = $\pm 1.6 \times 10^{-4}$ cP) as a function of mole fraction of lower alkanol in a typical binary mixture of 1-alkanols are depicted in Figures 2 and 3. Such figures

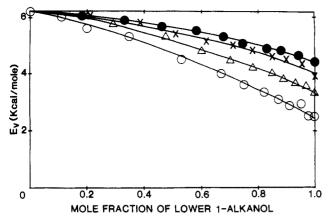


Figure 2. Viscous heat vs. mole fraction of lower 1-alkanol for binary mixtures of C₉ with C₁, C₂, C₃, and C₄: (O) C₁-C₉; (Δ) C₂-C₉; (X) $C_3 - C_9$; (\bullet) $C_4 - C_9$.

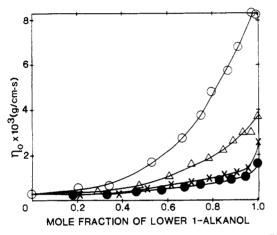


Figure 3. Preexponential factor vs. mole fraction of lower 1-alkanol for binary mixtures of C₉ with C₁, C₂, C₃, and C₄: (O) C₁-C₉; (Δ) C₂-C₉; $(X) C_3 - C_9; (\bullet) C_4 - C_9.$

for all mixtures investigated are available as supplementary material.

Glossarv

Α, Β. polynomial parameters C, D,

Ε

- M₁ molecular weight of the lower component in a binary mixture
- molecular weight of the higher component in a bi-Μ, nary mixture

- molar volume of a sample
- V1. V, molar volumes of lower and higher components, respectively, in a binary mixture
- \boldsymbol{X}_1 mole fraction of the lower component in a binary mixture
- X 2 mole fraction of the higher component in a binary mixture
- α_{12}, α_{21} interaction parameters
- coefficients which need to be determined by eq 2 β_{12}, β_{21} viscosity of a sample n
- viscosity of lower and higher components, respec- η_{1}, η_{2}
 - tively, in a binary mixture
- density of a sample ρ

Registry No. 1-Decanol, 112-30-1; 1-nonanol, 143-08-8; 1-octanol, 111-87-5; 1-heptanol, 111-70-6; 1-butanol, 71-36-3; 1-propanol, 71-23-8; ethanol, 64-17-5; methanol, 67-56-1.

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Supplementary Material Available: Table of rms errors for fits of viscosities of mixtures to various equations, and three figures for viscous heats and three figures for preexponential factors as functions of mole fractions of lower 1-alkanols in binary mixtures of 1-alkanols (9 pages). Ordering information is given on any current masthead page.

Solubility of Solid Acetic Acid in Liquid Organic Solvents

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The solubilities of acetic acid in some organic solvents (n-heptane, cyclopentane, carbon tetrachloride, toluene, chloroform, ethyl acetoacetate, methanol, ethanol, and acetone) have been measured for temperatures ranging from melting point to --30 °C. The results are compared with those predicted with UNIFAC and those calculated with the NRTL equation (vapor-liquid equilibrium (VLE) parameters).

Introduction

The experimental measurements of vapor-liquid (VLE), liquid-liquid (LLE), and liquid-solid equilibria available provide an abundance of information both theoretical and of interest in process design. While numerous experimental data are readily available for the first two types of equilibria (VLE and LLE), this is not so for liquid-solid equilibria (1, 2).